



Model-Based Rigorous Uncertainty Quantification in Complex Systems

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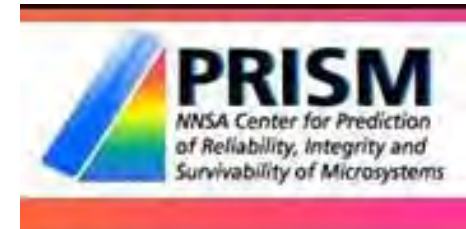
California Institute of Technology

COMPLAS 2011

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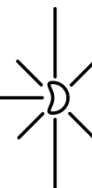
ASC/PSAAP Centers

CALTECH
PSAAP



CALTECH
PSAAP





Experimental

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G. Ravichandran
M. Adams
J. Mihaly
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Software

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M. Stalzer
M. McKerns
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J. Lindheim
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Management

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UQ

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Fluids

D. Meiron
D. Pullin
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A. L. Ortega

Solids

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K. Bhattacharya
W. A. Goddard III
A. van de Walle
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L. Perotti
D. Kochmann

The Quantification of Margins and Uncertainties (QMU) Paradigm



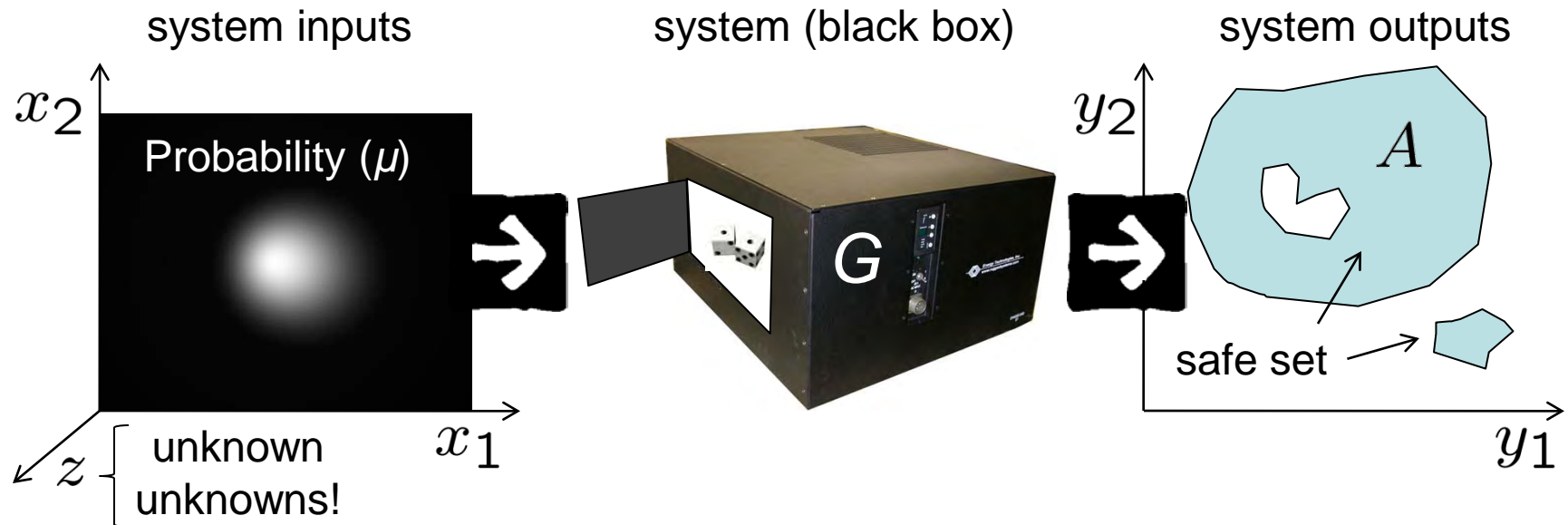
- Aim: *Predict mean performance and **uncertainty** in the behavior of complex physical/engineered systems*
- **Paradigm shift** in experimental science, modeling and simulation, scientific computing (***predictive science***):
 - Deterministic → Non-deterministic systems
 - Mean performance → Mean performance + Uncertainty



Old single-calculation paradigm



New ensemble-of-calculations
paradigm (QMU)



- Certification: PoF of the system below tolerance,

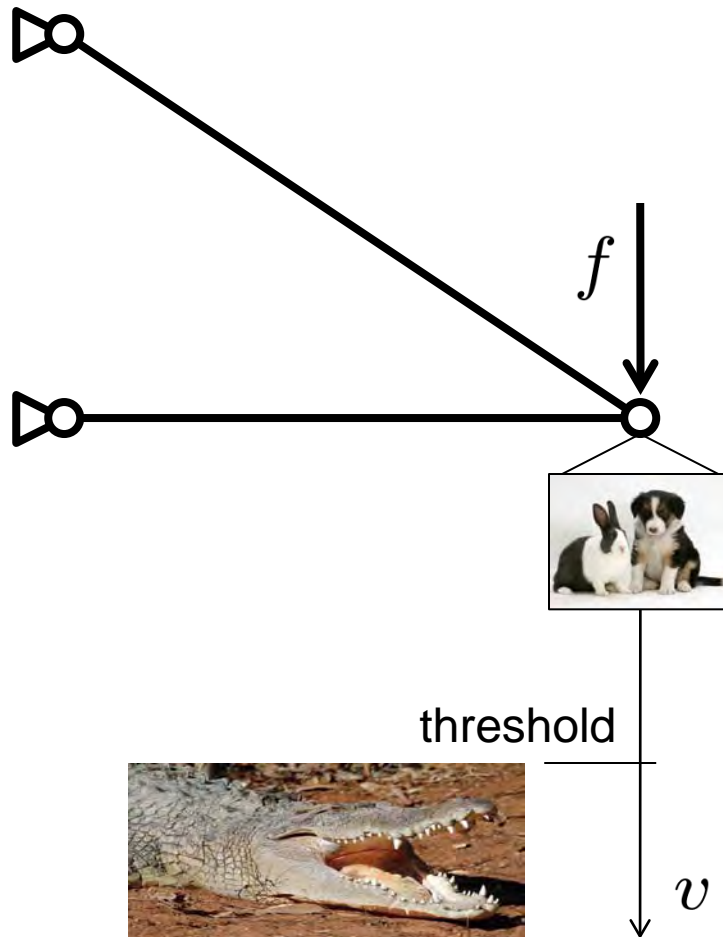
$$\mathbb{P}[\text{failure}] = \mathbb{P}[y \notin A] \leq \epsilon$$

- Exact probability of failure:

$$\mathbb{P}[\text{failure}] = \int \left\{ \begin{array}{ll} 0, & \text{if } G(x) \in A \\ 1, & \text{if } G(x) \notin A \end{array} \right\} d\mu(x)$$



QMU – A simple truss example



- System input: Applied force (f)
- System output: Tip deflection (v)
- Response function (G): Energy minimization, static equilibrium
- Model (F): Energy minimization with approximate strain-energy density function W
- Failure criterion: $v > \text{threshold}$
- To compute: $\mathbb{P}[\text{failure}] =$

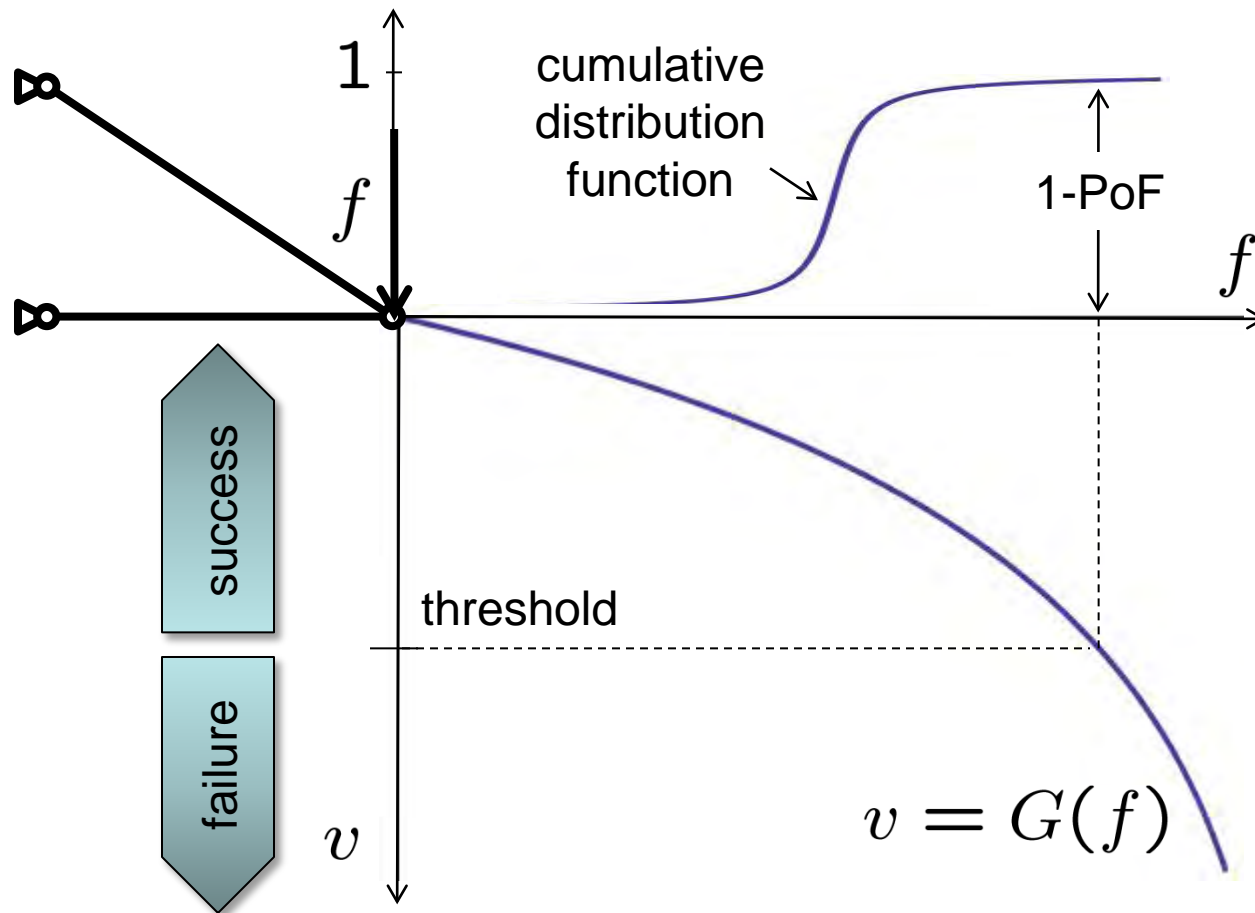
$$\int \left\{ \begin{array}{ll} 0, & \text{if } v < v_{\max} \\ 1, & \text{if } v \geq v_{\max} \end{array} \right\} d\mu(f)$$



QMU – A simple truss example



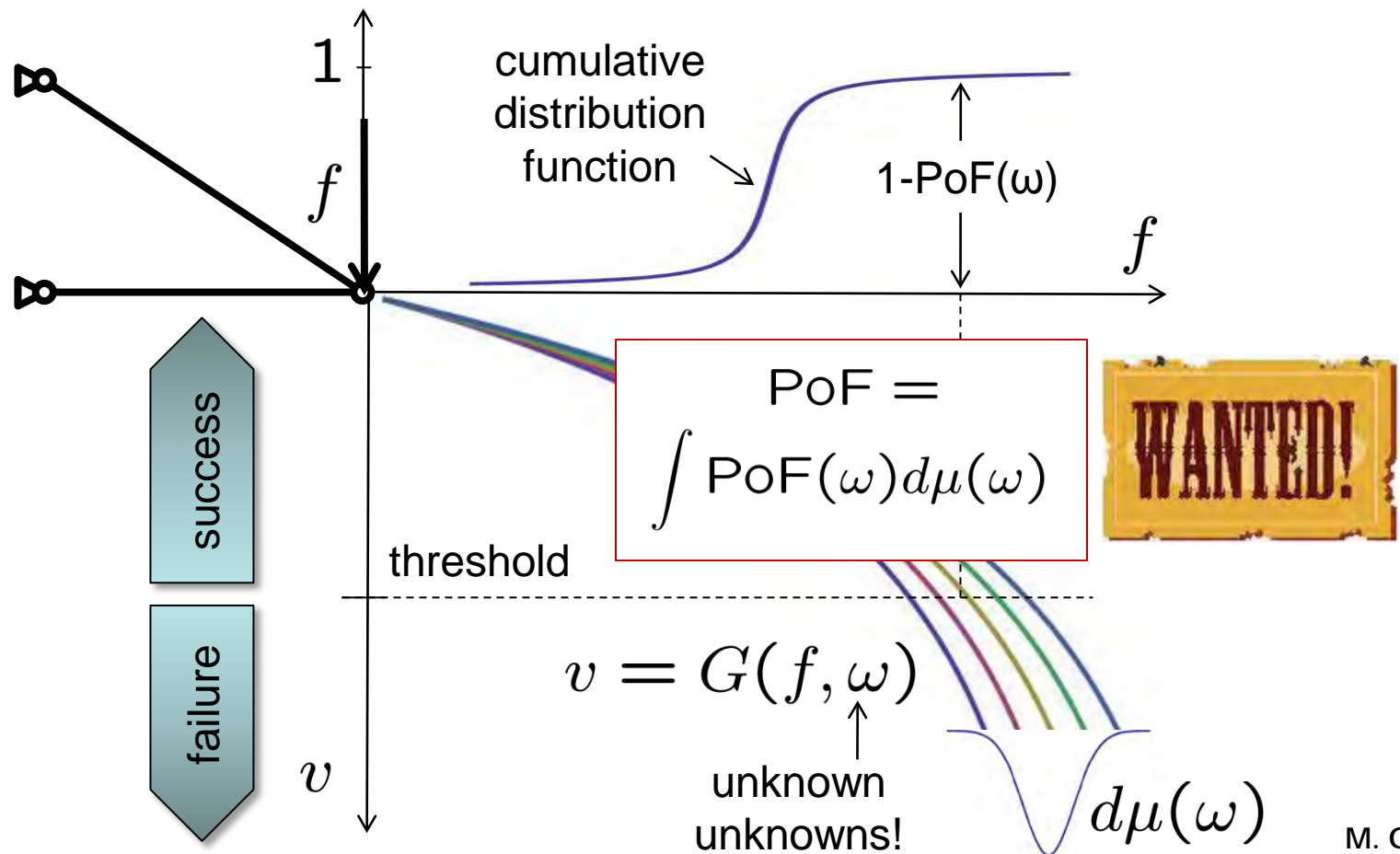
- Assume: Deterministic response, known probability distribution of inputs

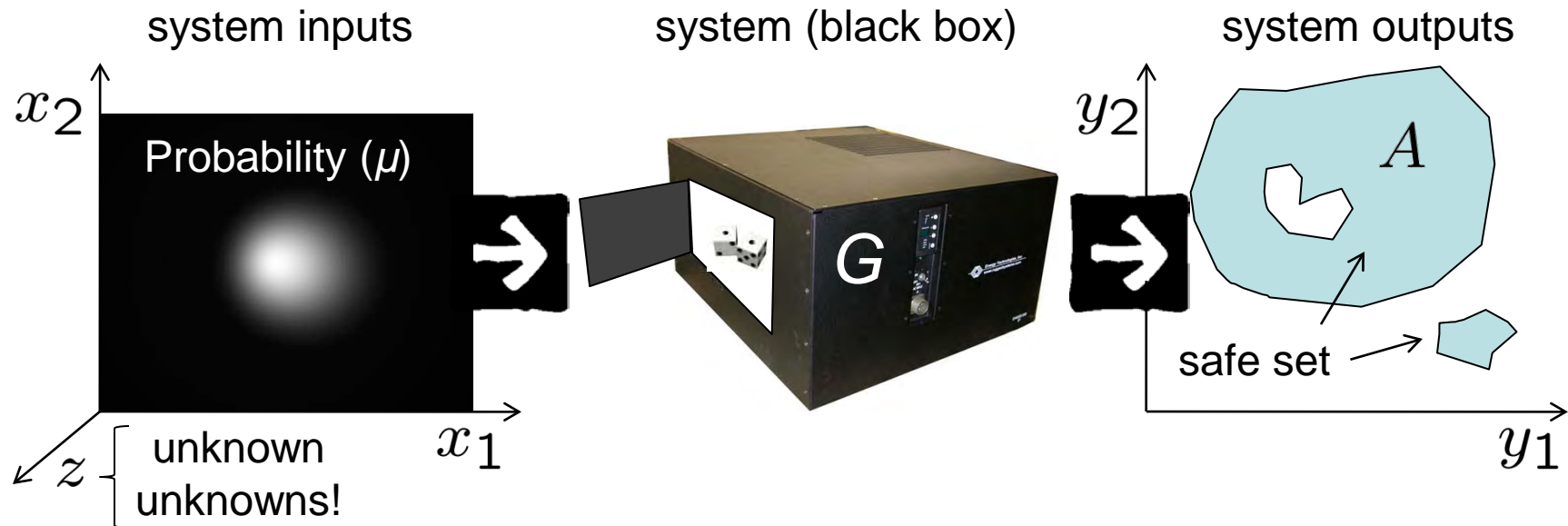


QMU – A simple truss example



- Assume: Stochastic response function, known probability distribution of inputs





- Certification: PoF of the system below tolerance,

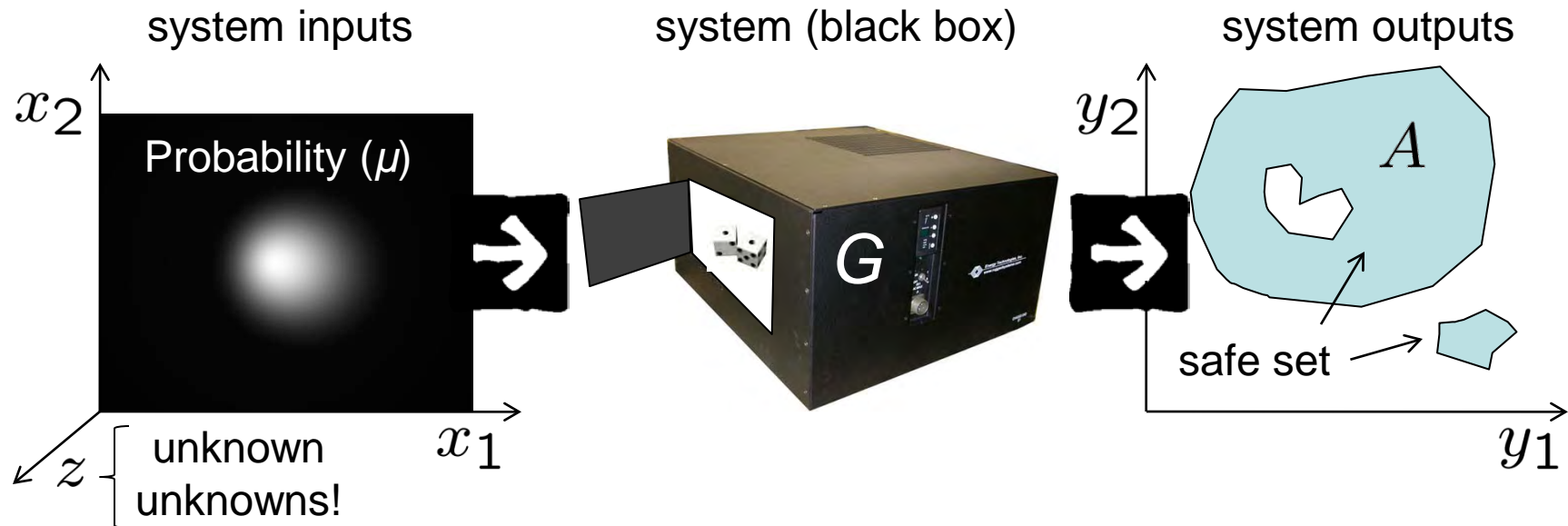
$$\mathbb{P}[\text{failure}] = \mathbb{P}[y \notin A] \leq \epsilon$$

- Exact probability of failure:

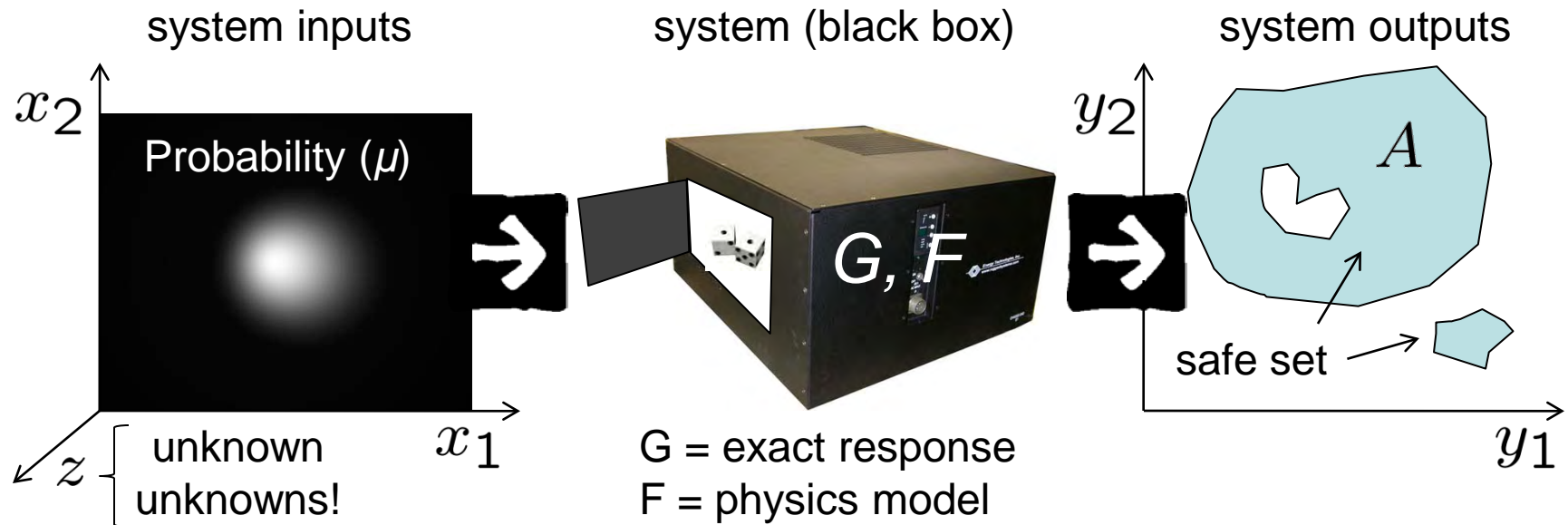
$$\mathbb{P}[\text{failure}] = \int \left\{ \begin{array}{ll} 0, & \text{if } G(x) \in A \\ 1, & \text{if } G(x) \notin A \end{array} \right\} d\mu(x)$$



QMU – Essential difficulties



- Input space of high dimension, unknown unknowns
- Probability distribution of inputs not known in general
- System response stochastic, not known in general
- Models are inaccurate, partially verified & validated
- System performance cannot be tested on demand
- Legacy data incomplete, inconsistent, and noisy...



- Conservative certification: **Upper bound** on the PoF of the system below tolerance,

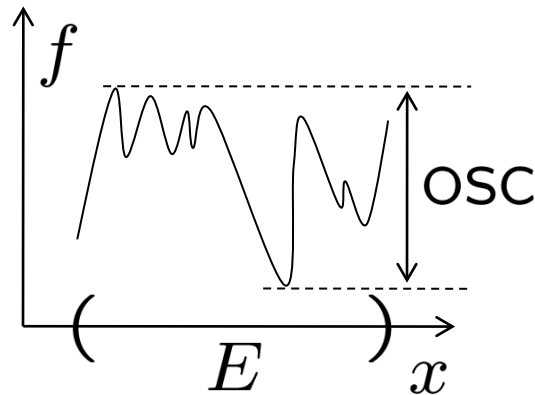
$$\mathbb{P}[\text{failure}] = \mathbb{P}[y \notin A] \leq \text{upper bound} \leq \epsilon$$

- Objective: Obtain tight (optimal?) PoF **upper bounds** from all known information about the system...

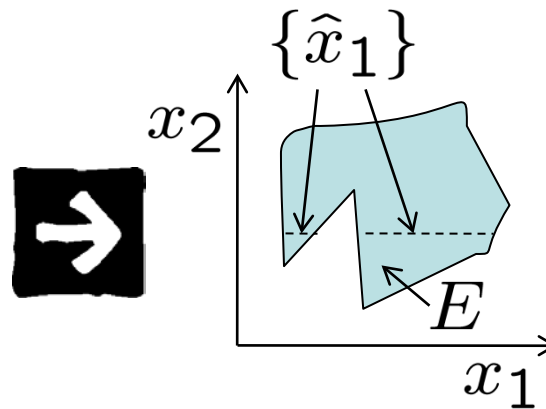
Example – McDiarmid’s inequality



- Function diameters:



One-dimensional diameter



Multidimensional diameter

computation requires
global optimization
over parameter space!

\rightarrow $|f|_D$

- McDiarmid’s CoM inequality: $\mathbb{P}[\text{failure}] \leq e^{-2(M/U)^2}$

$M \equiv \text{margin} = \text{mean output} - \text{threshold} - \text{margin hit}$

$U \equiv \text{uncertainty} = \underbrace{\text{predicted}}_{|F|_D} + \underbrace{\text{modeling}}_{|F - G|_D} + \underbrace{\text{scatter}}_{\sim 2\sigma}$

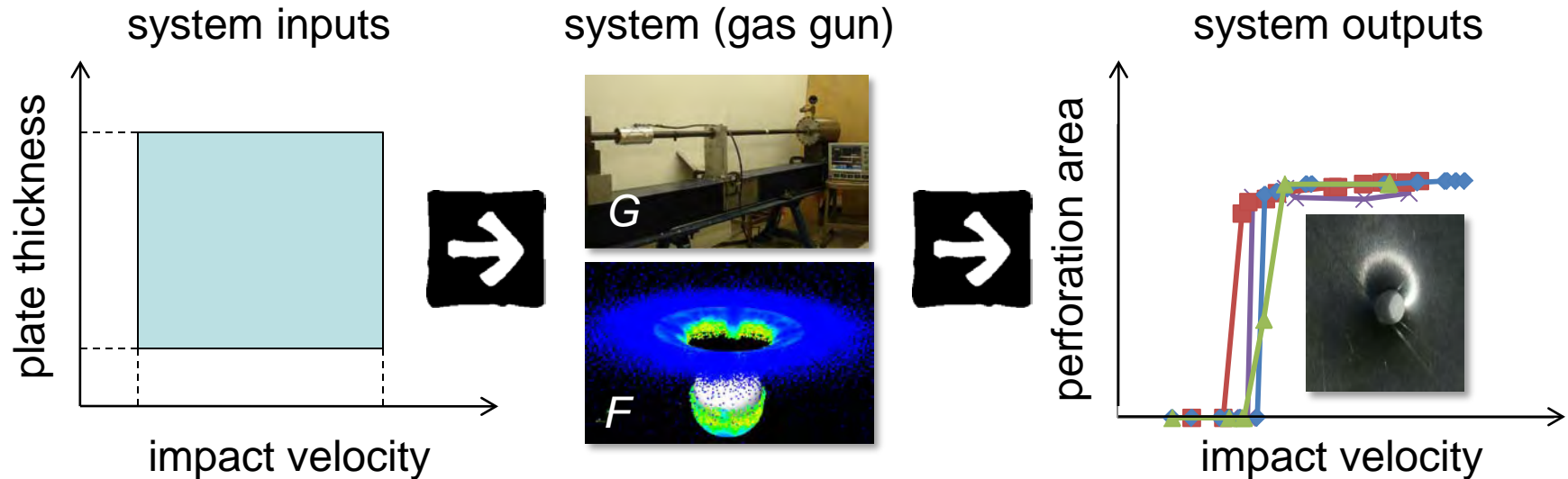
Lucas, Owhadi & MO
CMAME (2008)

$|F|_D$
model
diameter

$|F - G|_D$
modeling error
diameter

$\sim 2\sigma$

Example: Certifying threat lethality

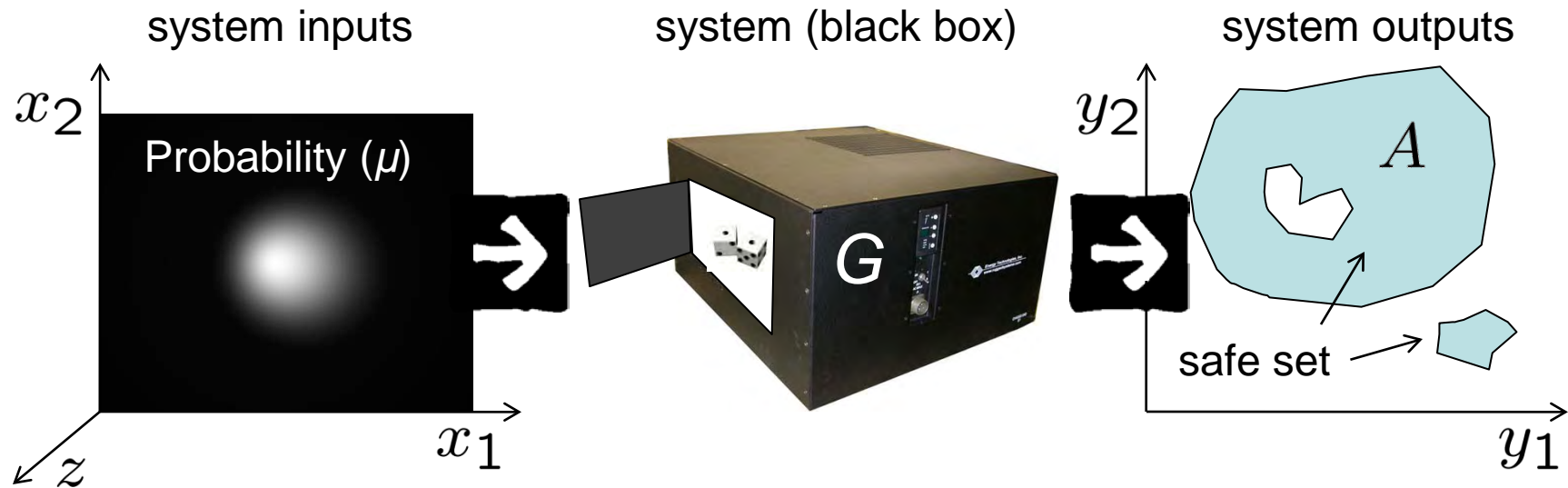


Model diameter $ F _D$	6.24 mm ²
Modeling error $ F-G _D$	5.41 mm ²
Experimental scatter 2σ	0.50 mm ²
Uncertainty $ F _D + F-G _D + 2\sigma$	11.65 mm ²
Empirical mean $\langle G \rangle$	47.77 mm ²
Margin hit α ($\epsilon' = 0.1\%$)	4.17 mm ²
Confidence factor M/U	<u>3.59</u>

- System certified with very high confidence (PoF < 0.1%)
- Total number of tests required ~ 50
- Total number of calculations ~ 2000

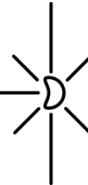


- Rigorous and conservative certification can be achieved by means of PoF upper bounds!
- PoF bounds ‘fold in’ all information available on the system (experimental data, V&V’d physics models...)
- PoF bounds are similar in spirit to bounds on effective moduli of elastic composites (which cannot be obtained exactly in general from existing data on the composite)
- However: Bounds can be suboptimal (e.g., Voigt, Reuss...) and result in excessive conservatism
- Question: Is it possible to compute optimal PoF bounds? (for given information about the system)
- **Optimal Uncertainty Quantification! (OUQ)**



- Wanted: $\mathbb{P}[\text{failure}] = \mathbb{E}_\mu[\{G \in A\}]$
- Assume information about (μ, G) : Data, models...
- Admissible set: $\mathcal{A} = \{(\mu, G) \text{ compatible with info}\}$
- Optimal PoF bounds given \mathcal{A} :

$$\inf_{(\mu, G) \in \mathcal{A}} \mathbb{E}_\mu(\{G \in A\}) \leq \text{PoF} \leq \sup_{(\mu, G) \in \mathcal{A}} \mathbb{E}_\mu(\{G \in A\})$$



Theorem [Owhadi *et al.* (2011)] Suppose that

$$\mathcal{A} = \left\{ (\mu, G) \left| \begin{array}{l} \langle \text{some conditions on } G \text{ alone} \rangle \\ \mathbb{E}_\mu[\varphi_1] \leq 0, \dots, \mathbb{E}_\mu[\varphi_n] \leq 0 \end{array} \right. \right\}. \text{ Let:}$$

$$\mathcal{A}_{\text{red}} = \left\{ (\mu, G) \in \mathcal{A} \left| \mu = \sum_{i=1}^n \alpha_i \delta_{x_i}, \alpha_i \geq 0, \sum_{i=1}^n \alpha_i = 1 \right. \right\}$$

$$\text{Then: } \inf_{(\mu, G) \in \mathcal{A}} \mathbb{E}_\mu(\{G \in A\}) = \inf_{(\mu, G) \in \underline{\mathcal{A}_{\text{red}}}} \mathbb{E}_\mu(\{G \in A\})$$

$$\sup_{(\mu, G) \in \mathcal{A}} \mathbb{E}_\mu(\{G \in A\}) = \sup_{(\mu, G) \in \underline{\mathcal{A}_{\text{red}}}} \mathbb{E}_\mu(\{G \in A\})$$

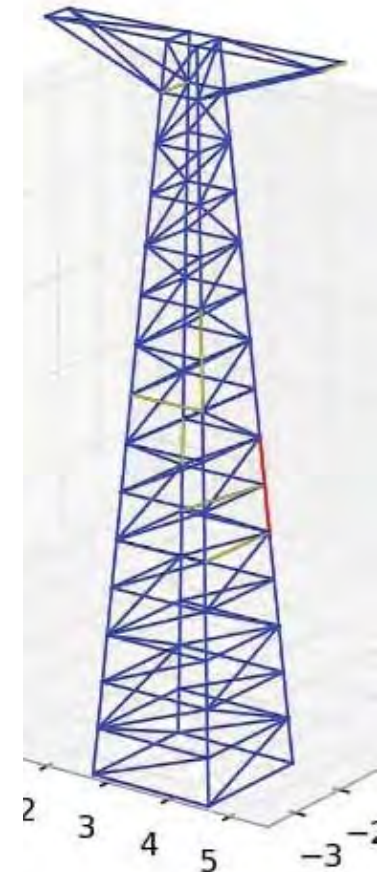
- OUQ problem is reduced to optimization over finite-dimensional space of measures: Program feasible!

M. Ortiz

Example – Seismic risk assessment



Simulation of seismic waves from rupture initiating at Parkfield, central California, and propagating over Los Angeles basin (<http://krishnan.caltech.edu/krishnan/res.html>)



3D truss structure of power-line tower

Example – Seismic risk assessment



- Ground motion acceleration:

$$\ddot{u}_0(t) = (\psi * s)(t)$$

where: $s(t) \equiv$ Source activity

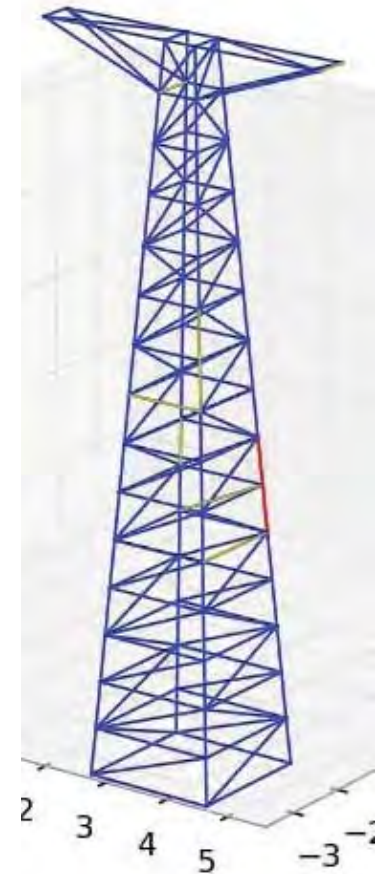
$\psi(t) \equiv$ Transfer function

- Structural response:

$$M\ddot{u} + C\dot{u} + Ku = f(t) - MT\ddot{u}_0(t)$$

- Failure criterion: $G \leq 0$, where

$$G = \min_{i \in \text{members}} \left\{ \sigma_y - \max_{t \geq 0} |\sigma_i(t)| \right\}$$

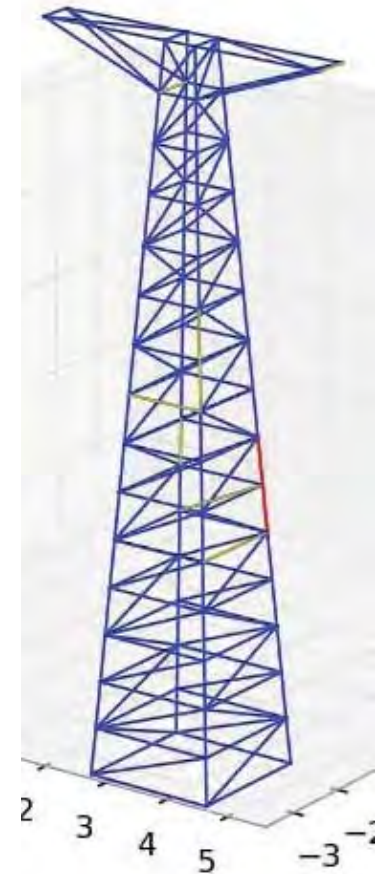


3D truss structure
of power-line tower

Example – Seismic risk assessment

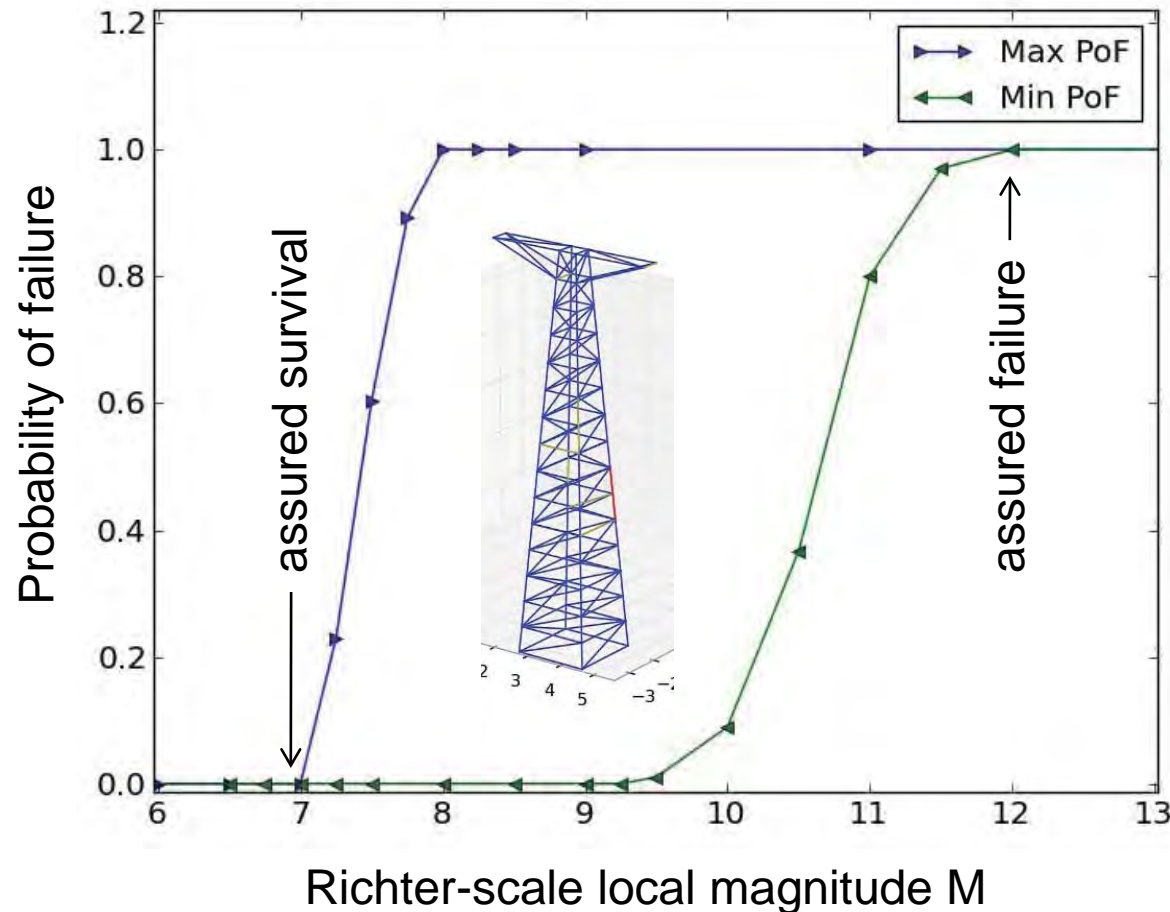


- Assumptions on source term $s(t)$:
 - Piecewise constant in time
 - Random amplitudes in $[-a_{\max}, a_{\max}]$ (given by Richter magnitude M) with zero mean
 - Random time interval durations with bounded mean
- Assumptions on transfer function $\psi(t)$:
 - Piecewise linear in time
 - Random amplitudes with zero mean, bounded L^2 norm
- Reduced OUQ problem: Global optimization in 179 dimensions
- One PoF calculation takes $O(24 \text{ hours})$ on $O(1000)$ AMD opteron cluster



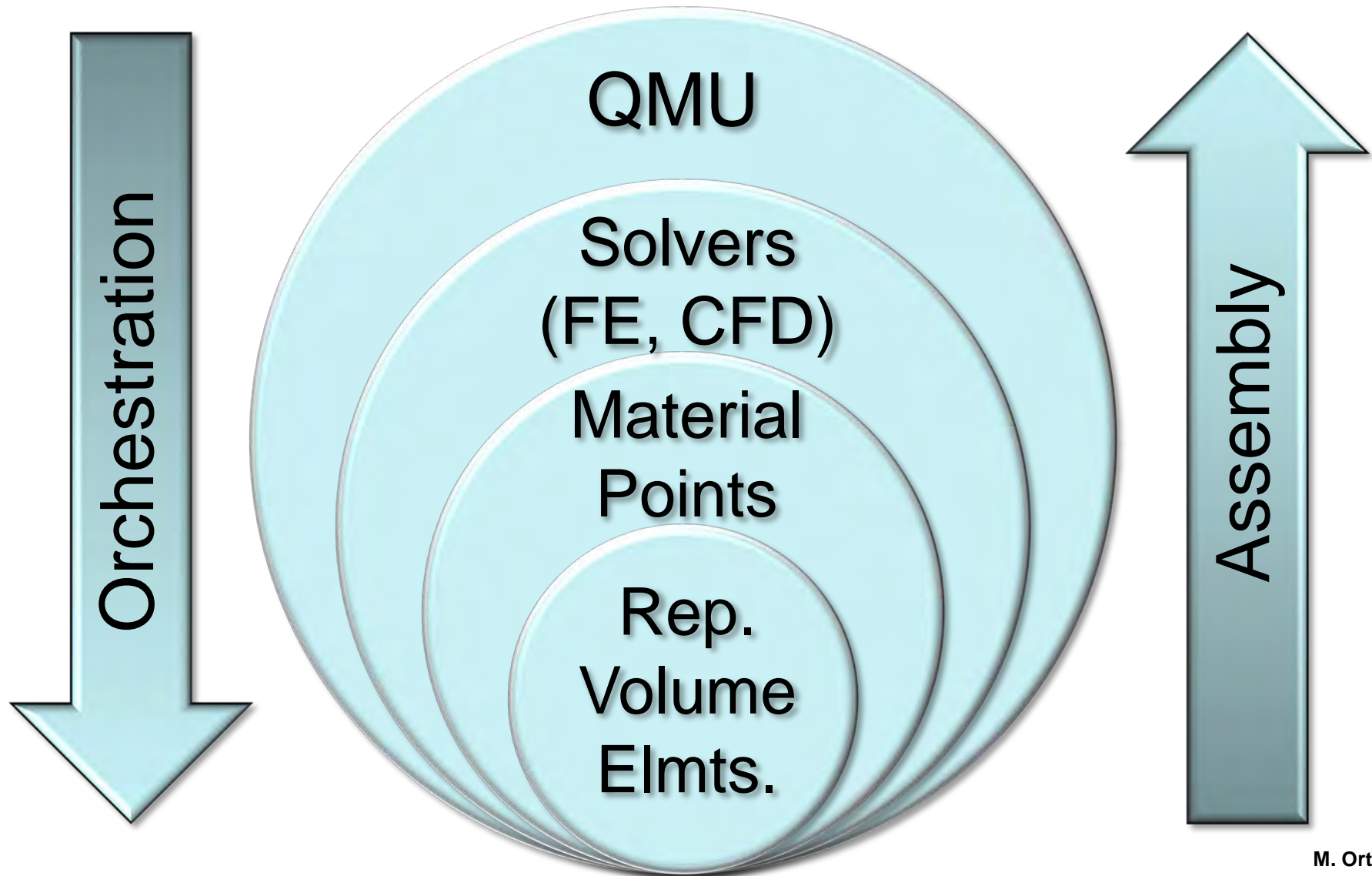
3D truss structure
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Example – Seismic risk assessment

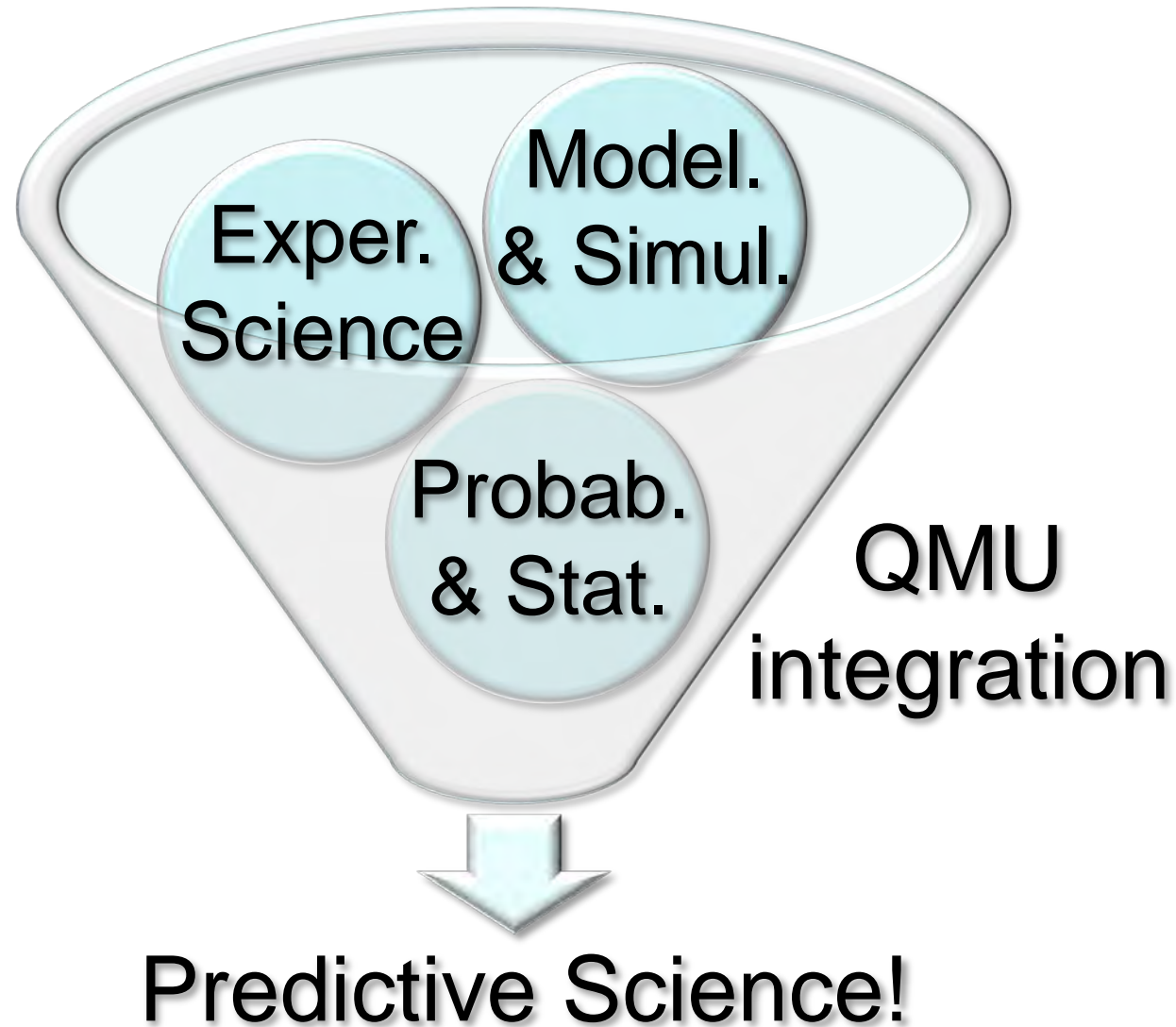


Optimal PoF upper and lower bounds vs. Richter scale magnitude M
at hypocentral distance $R=25$ km, with a_{\max} given by Esteva's
semi-empirical expression as a function of M

Concluding remarks – Systems view of Computational Mechanics...



Concluding remarks – Disciplinary view of QMU and Predictive Science



Concluding remarks...



Thank you!